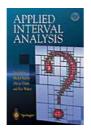
# Interval analysis for robust control; application to sailboat robotics

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Journée scientifique en hommage à Éric Walter
Jeudi 20 mars 2014.





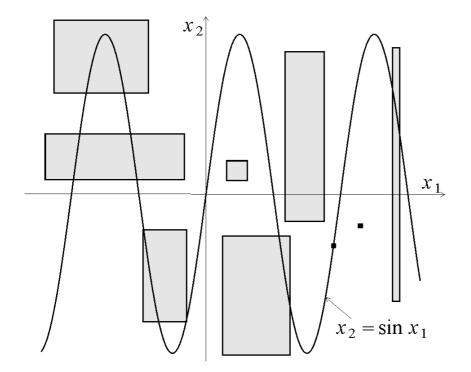
# 1 Contractors

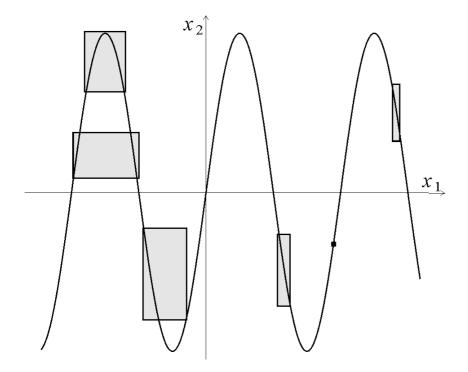
The operator  $\mathcal{C}:\mathbb{IR}^n\to\mathbb{IR}^n$  is a *contractor* for the equation  $f(\mathbf{x})=0,$  if

$$\left\{ \begin{array}{l} \mathcal{C}([\mathbf{x}]) \subset [\mathbf{x}] & \text{(contractance)} \\ \mathbf{x} \in [\mathbf{x}] \text{ and } f(\mathbf{x}) = \mathbf{0} \Rightarrow \mathbf{x} \in \mathcal{C}([\mathbf{x}]) & \text{(consistence)} \end{array} \right.$$

**Example**. Consider the primitive equation:

$$x_2 = \sin x_1.$$





## Contractor algebra

intersection	$\left(\mathcal{C}_{1}\cap\mathcal{C}_{2}\right)\left(\left[\mathbf{x} ight] ight)\overset{def}{=}\mathcal{C}_{1}\left(\left[\mathbf{x} ight] ight)\cap\mathcal{C}_{2}\left(\left[\mathbf{x} ight] ight)$
union	$\left(\mathcal{C}_{1}\cup\mathcal{C}_{2} ight)\left(\left[\mathbf{x} ight] ight)\overset{def}{=}\left[\mathcal{C}_{1}\left(\left[\mathbf{x} ight] ight)\cup\mathcal{C}_{2}\left(\left[\mathbf{x} ight] ight) ight]$
composition	$(\mathcal{C}_1 \circ \mathcal{C}_2)([\mathbf{x}]) \stackrel{def}{=} \mathcal{C}_1(\mathcal{C}_2([\mathbf{x}]))$
reiteration	$\mathcal{C}^{\infty} \stackrel{def}{=} \mathcal{C} \circ \mathcal{C} \circ \mathcal{C} \circ \ldots$

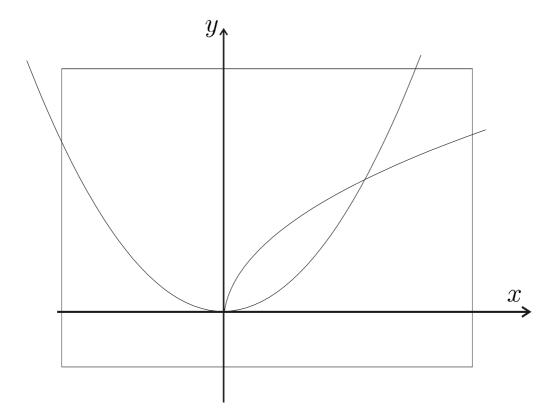
## **Example.** Solve the system

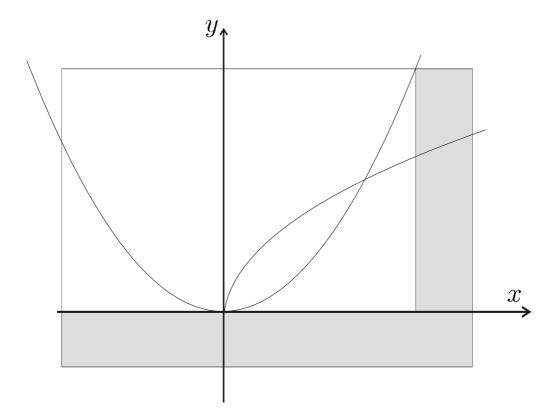
$$y = x^2$$
$$y = \sqrt{x}.$$

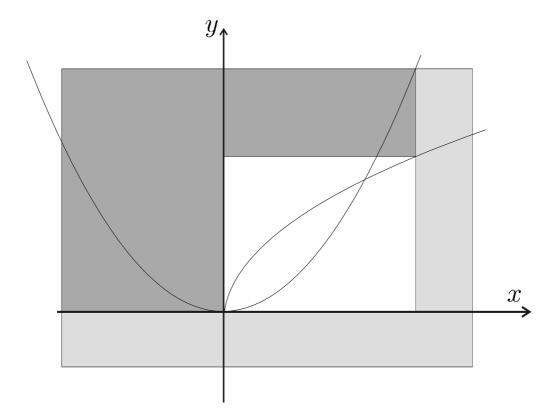
We build two contractors

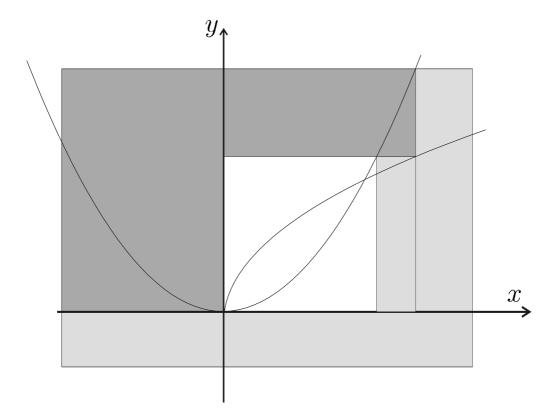
$$C_1: \left\{ \begin{array}{l} [y] = [y] \cap [x]^2 \\ [x] = [x] \cap \sqrt{[y]} \end{array} \right.$$
 associated with  $y = x^2$ 

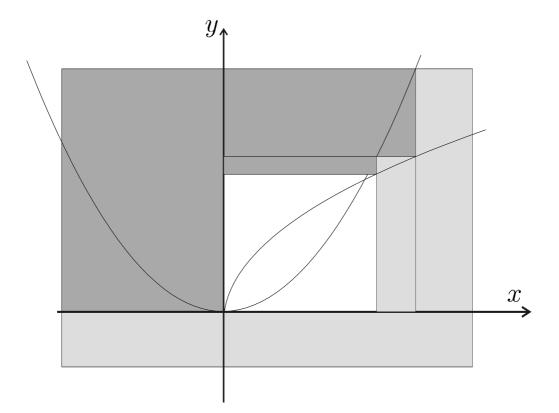
$$C_2: \left\{ \begin{array}{l} [y] = [y] \cap \sqrt{[x]} \\ [x] = [x] \cap [y]^2 \end{array} \right.$$
 associated with  $y = \sqrt{x}$ 

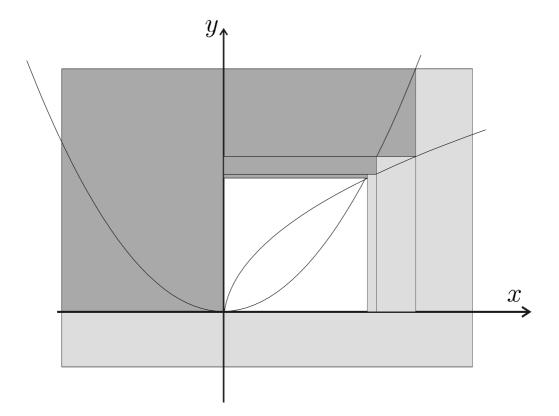


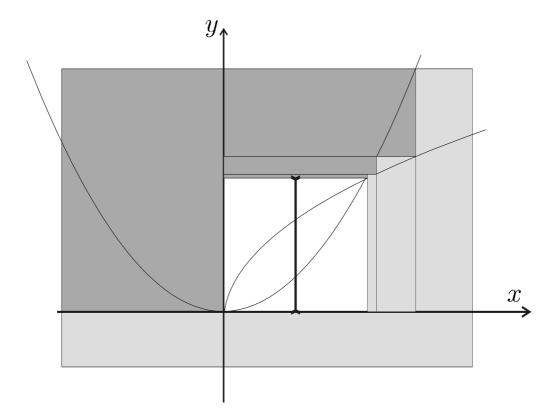


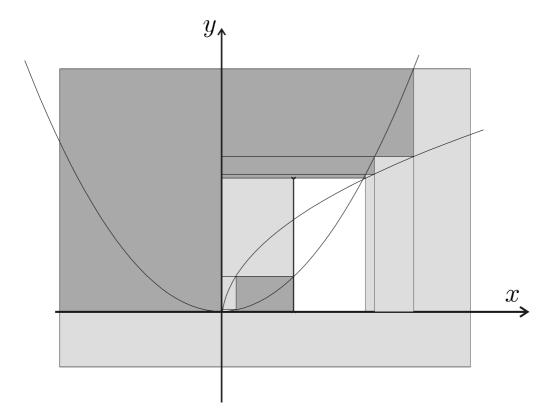


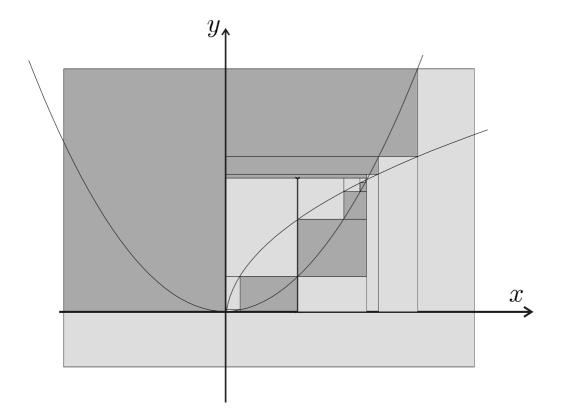








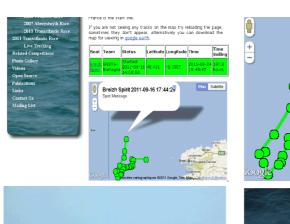




## 2 Sailboat robotics

















## 3 Vaimos

 ${\bf Collaboration~ENSTA/IFREMER}$ 



Vaimos à la WRSC (ENSTA-IFREMER-Ecole Navale).

$$\begin{cases} \dot{x} &= v \cos \theta + p_1 a \cos \psi \\ \dot{y} &= v \sin \theta + p_1 a \sin \psi \\ \dot{\theta} &= \omega \\ \dot{v} &= \frac{f_s \sin \delta_s - f_r \sin u_1 - p_2 v^2}{p_9} \\ \dot{\omega} &= \frac{f_s (p_6 - p_7 \cos \delta_s) - p_8 f_r \cos u_1 - p_3 \omega}{p_{10}} \\ f_s &= p_4 a \sin (\theta - \psi + \delta_s) \\ f_r &= p_5 v \sin u_1 \\ \sigma &= \cos (\theta - \psi) + \cos (u_2) \\ \delta_s &= \begin{cases} \pi - \theta + \psi & \text{si } \sigma \leq 0 \\ sign (\sin (\theta - \psi)) . u_2 & \text{sinon.} \end{cases} \end{cases}$$

The robot satisfies a state equation

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u})$$
.

With the controller  $\mathbf{u} = \mathbf{g}(\mathbf{x})$ , the robot satisfies

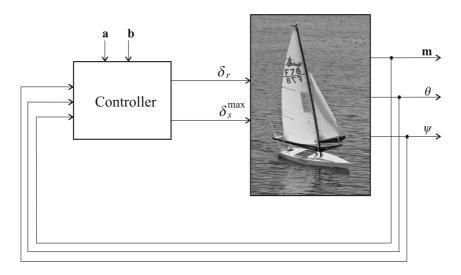
$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$$
.

With all uncertainties, the robot satisfies.

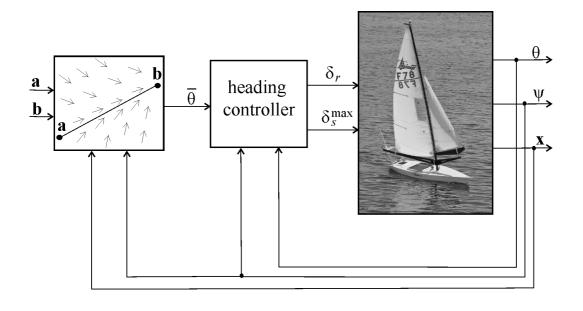
$$\mathbf{\dot{x}}\in\mathbf{F}\left(\mathbf{x}\right)$$

which is a differential inclusion.

4 Line following



Controller of a sailboat robot

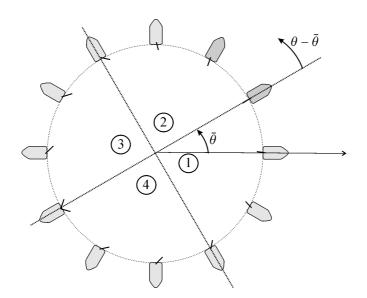


#### **Heading controller**

$$\begin{cases} \delta_r &= \frac{\delta_r^{\max}}{\pi}.\operatorname{atan}(\tan\frac{\theta-\overline{\theta}}{2}) \\ \delta_s^{\max} &= \frac{\pi}{2}.\left(\frac{\cos(\psi-\overline{\theta})+1}{2}\right). \end{cases}$$

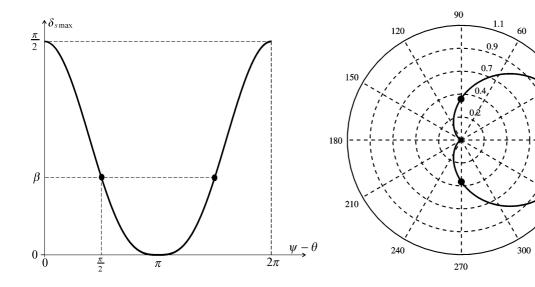
#### Rudder

$$\left\{ \delta_r = \frac{\delta_r^{\mathsf{max}}}{\pi}.\mathsf{atan}(\mathsf{tan}\,\frac{\theta-\bar{\theta}}{2}) \right.$$

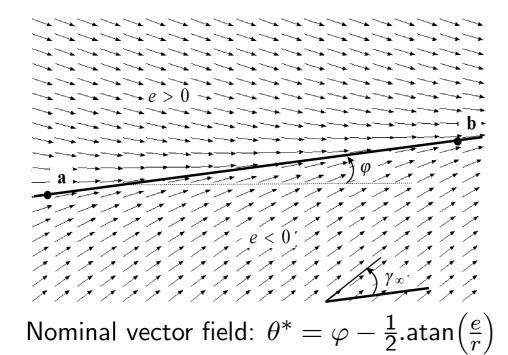


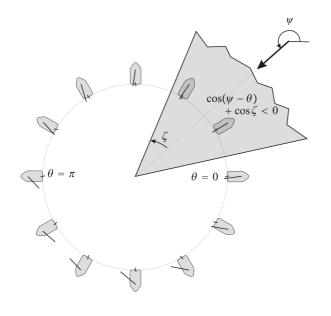
#### Sail

$$\delta_s^{\mathsf{max}} = rac{\pi}{2} \cdot \left( rac{\mathsf{cos}\left(\psi - \overline{ heta}
ight) + 1}{2} 
ight)$$

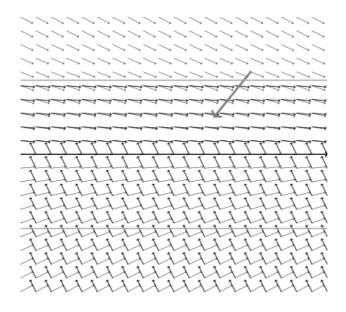


### 4.1 Vector field





A course  $\theta^*$  may be unfeasible



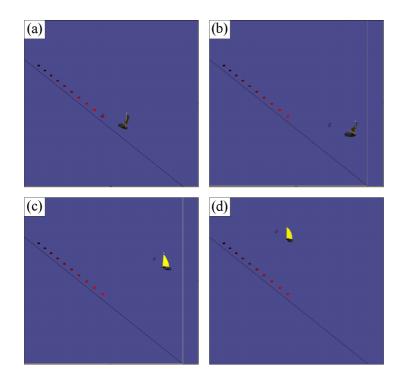
Keep close hauled strategy.

## 4.2 Controller

Controlleur : in:  $\mathbf{m}, \theta, \psi, \mathbf{a}, \mathbf{b}$ ; out:  $\delta_r, \delta_s^{\text{max}}$ ; inout: q  $1 \quad e = \frac{\det(\mathbf{b} - \mathbf{a}, \mathbf{m} - \mathbf{a})}{\|\mathbf{b} - \mathbf{a}\|}$ 

- if  $|e|>rac{\ddot{r'}}{2}$  then  $q=\mathsf{sign}(e)$
- $\overline{ heta} = \operatorname{atan2}(\mathbf{b} \mathbf{a}) \frac{1}{2}.\operatorname{atan}(\frac{e}{r})$
- 4 if  $\cos\left(\psi \bar{\theta}\right) + \cos\zeta < 0$  then  $\bar{\theta} = \pi + \psi q.\zeta$ . 5  $\delta_r = \frac{\delta_r^{\text{max}}}{\pi}.\text{atan}(\tan\frac{\theta \bar{\theta}}{2})$
- 6  $\delta_s^{\mathsf{max}} = \frac{\pi}{2} \cdot \left( \frac{\cos(\psi \bar{\theta}) + 1}{2} \right)$ .





## 6 Theoretical validation

\*Jaulin, Le Bars (2012). An interval approach for stability analysis; Application to sailboat robotics. IEEE TRO.

When the wind is known, the sailboat with the heading controller is described by

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}).$$

The system

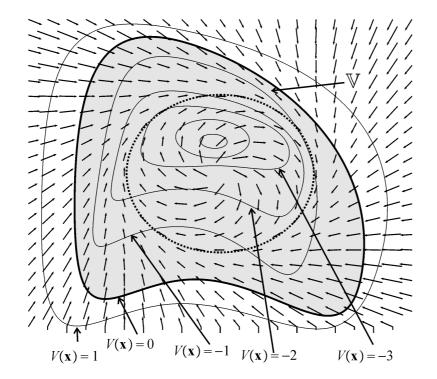
$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$$

is Lyapunov-stable (1892) is there exists  $V\left(\mathbf{x}\right) \geq \mathbf{0}$  such that

$$\dot{V}(\mathbf{x}) < 0 \text{ if } \mathbf{x} \neq \mathbf{0},$$
 $V(\mathbf{x}) = 0 \text{ iff } \mathbf{x} = \mathbf{0}.$ 

**Definition**. Consider a differentiable function  $V(\mathbf{x}) : \mathbb{R}^n \to \mathbb{R}$ . The system  $\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$  is V-stable if

$$(V(\mathbf{x}) \geq \mathbf{0} \Rightarrow \dot{V}(\mathbf{x}) \leq \varepsilon < \mathbf{0}).$$



**Theorem**. If the system  $\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$  is V-stable then

- (i)  $\forall \mathbf{x}(0), \exists t \geq 0 \text{ such that } V(\mathbf{x}(t)) < 0$
- (ii) if  $V(\mathbf{x}(t)) < 0$  then  $\forall \tau > 0$ ,  $V(\mathbf{x}(t+\tau)) < 0$ .

Now,

$$\begin{pmatrix} V(\mathbf{x}) \geq 0 \Rightarrow \dot{V}(\mathbf{x}) < 0 \end{pmatrix}$$

$$\Leftrightarrow \begin{pmatrix} V(\mathbf{x}) \geq 0 \Rightarrow \frac{\partial V}{\partial \mathbf{x}}(\mathbf{x}) \cdot \mathbf{f}(\mathbf{x}) < 0 \end{pmatrix}$$

$$\Leftrightarrow \forall \mathbf{x}, \frac{\partial V}{\partial \mathbf{x}}(\mathbf{x}) \cdot \mathbf{f}(\mathbf{x}) < 0 \text{ or } V(\mathbf{x}) < 0$$

$$\Leftrightarrow \neg \left( \exists \mathbf{x}, \frac{\partial V}{\partial \mathbf{x}}(\mathbf{x}) \cdot \mathbf{f}(\mathbf{x}) \geq 0 \text{ and } V(\mathbf{x}) \geq 0 \right)$$

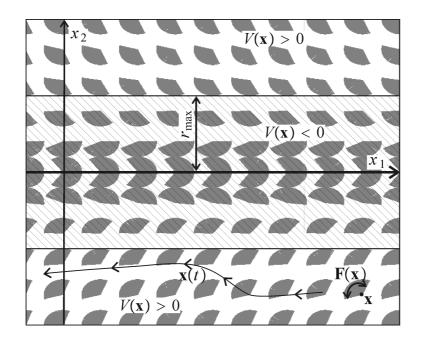
Theorem. We have

$$\left\{ \begin{array}{l} \frac{\partial V}{\partial \mathbf{x}} \left( \mathbf{x} \right) . \mathbf{f} \left( \mathbf{x} \right) \geq \mathbf{0} \\ V(\mathbf{x}) \geq \mathbf{0} \end{array} \right. \text{ inconsistent } \Leftrightarrow \mathbf{\dot{x}} = \mathbf{f} \left( \mathbf{x} \right) \text{ is $V$-stable}.$$

Interval method could easily prove the  $V\mbox{-stability}.$ 

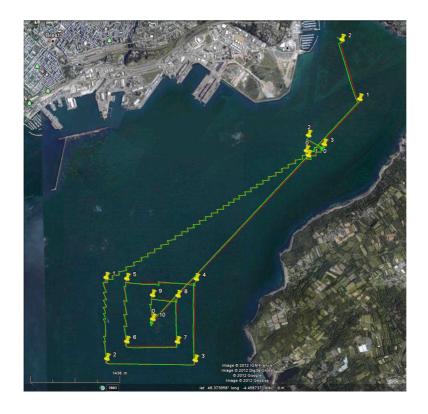
Theorem. We have

$$\begin{cases} \frac{\partial V}{\partial \mathbf{x}}(\mathbf{x}) . \mathbf{a} \geq \mathbf{0} \\ \mathbf{a} \in \mathbf{F}(\mathbf{x}) & \text{inconsistent } \Leftrightarrow \ \dot{\mathbf{x}} \in \mathbf{F}(\mathbf{x}) \ \text{is $V$-stable} \\ V(\mathbf{x}) \geq \mathbf{0} \end{cases}$$



Differential inclusion  $\dot{\mathbf{x}} \in \mathbf{F}(\mathbf{x})$  for the sailboat.  $V(x) = x_2^2 - r_{\max}^2.$ 





Rade de Brest

Brest-Douarnenez. January 17, 2012, 8am

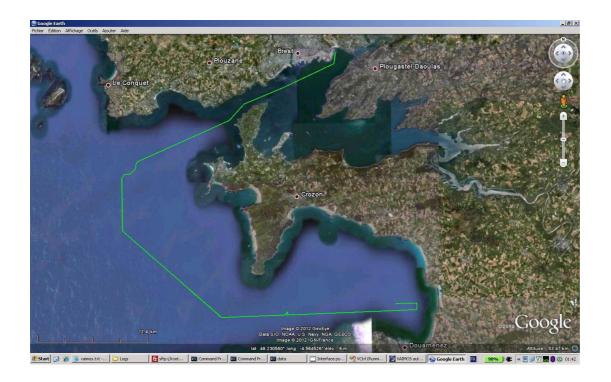


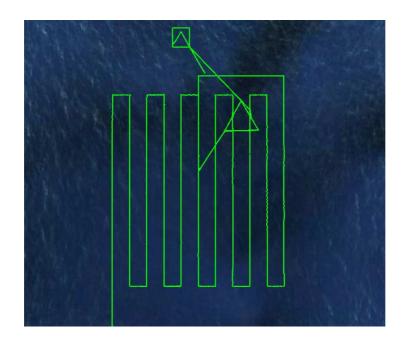












Middle of Atlantic ocean, 350 km made by Vaimos in 53h, September 6-9, 2012.

## Consequence.

It is possible for a sailboat robot to navigate inside a corridor.

Essential, to create circulation rules when robot swarms are considered.

Essential to determine who has to pay in case of accident.