

A Novel Application of Multivariable \mathcal{L}_1 Adaptive Control: from Design to Real-Time Implementation on an Underwater Vehicle

D. Maalouf, V. Creuze, and A. Chemori

OUTLINE

- I. Introduction: Problems/Challenges
- II. Proposed Control Scheme
- III. Dynamic Modeling
- IV. Experimental Results
- V. Conclusion



AC-ROV (Access Ltd)

- Actuation:**
- 6 thrusters
 - 5 actuated DOF
- Sensors:**
- IMU
 - Camera
 - Depth Sensor

Objective

Control of a small underwater vehicle in presence of parameter uncertainties and external disturbances.



Introduction

Controller

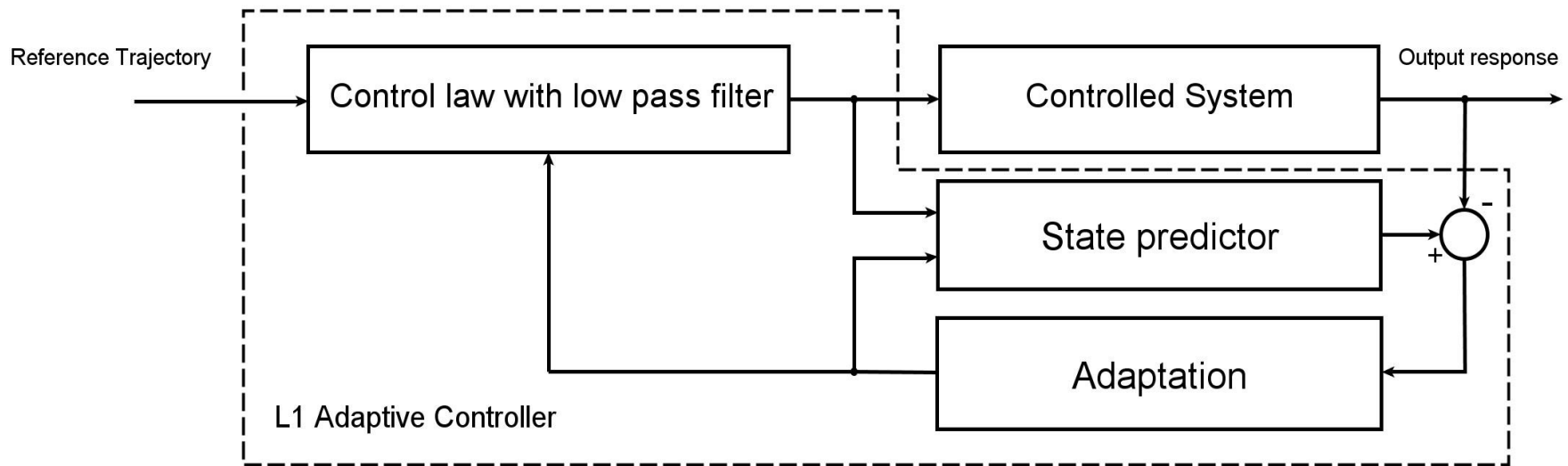
Modeling

Experiments

Conclusion

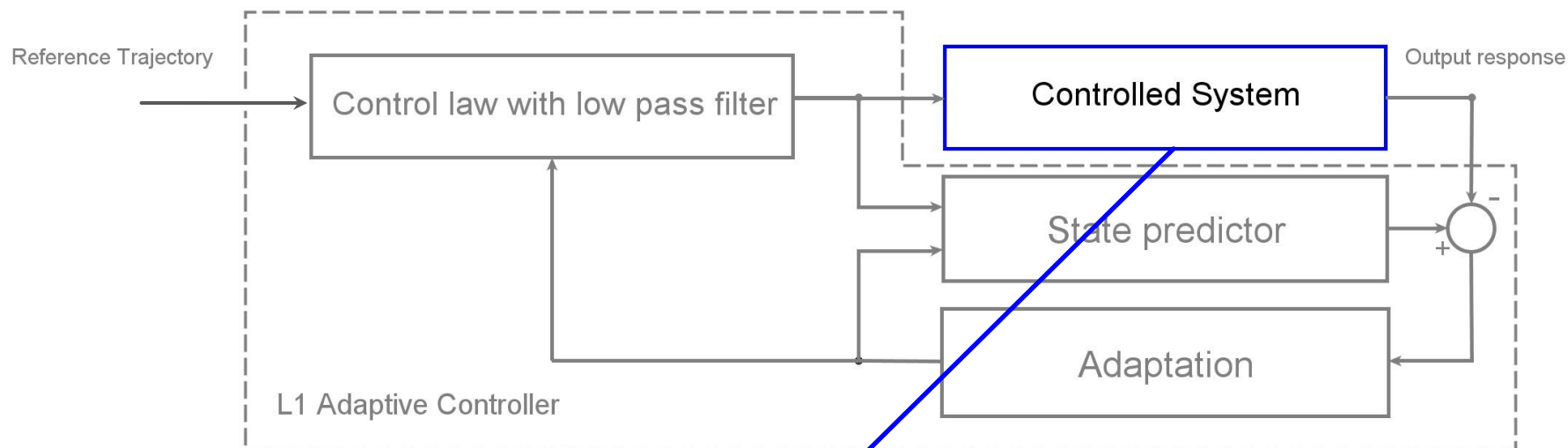
Controller

\mathcal{L}_1 Adaptive Controller Architecture



- Recently developed controller decoupling robustness and adaptation [Hovakimyan2010]
- Validated performance through experimental results in flight control
- Implemented in various systems mainly aerial vehicles but never in underwater ones

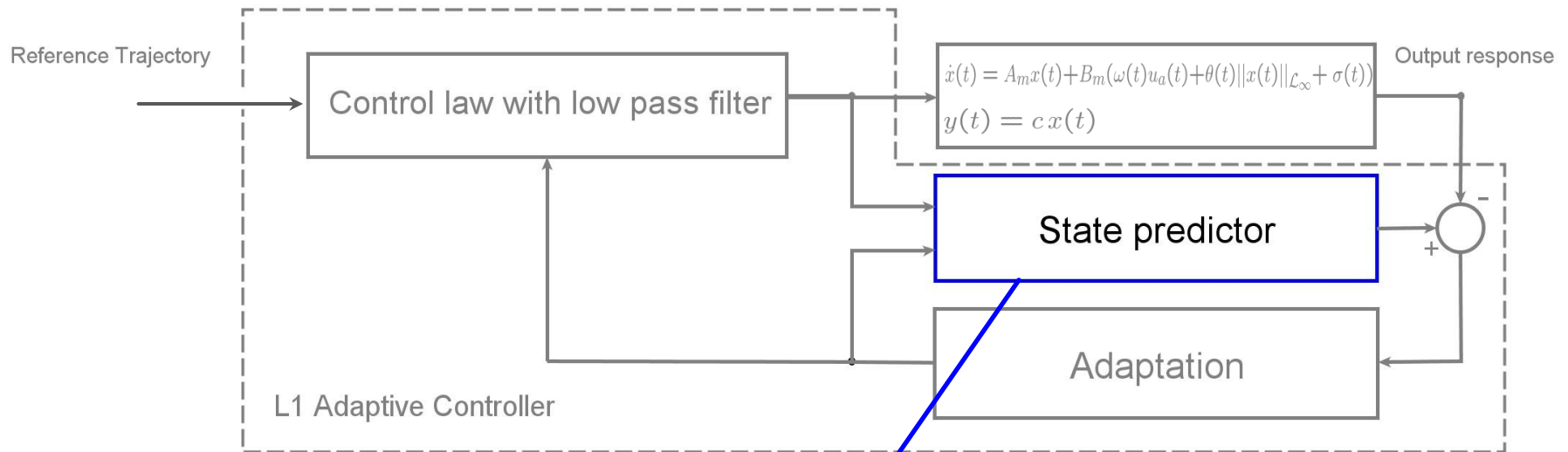
\mathcal{L}_1 Adaptive Controller Architecture



$$\dot{x}(t) = A \begin{cases} \dot{x}_1(t) = x_2(t) \\ \dot{x}_2(t) = f_2(t, x(t)) + B_2 \omega u \end{cases} \quad \|x(t)\|_{\mathcal{L}_\infty} + \sigma(t)$$

$$y(t) = C \quad y(t) = Cx(t)$$

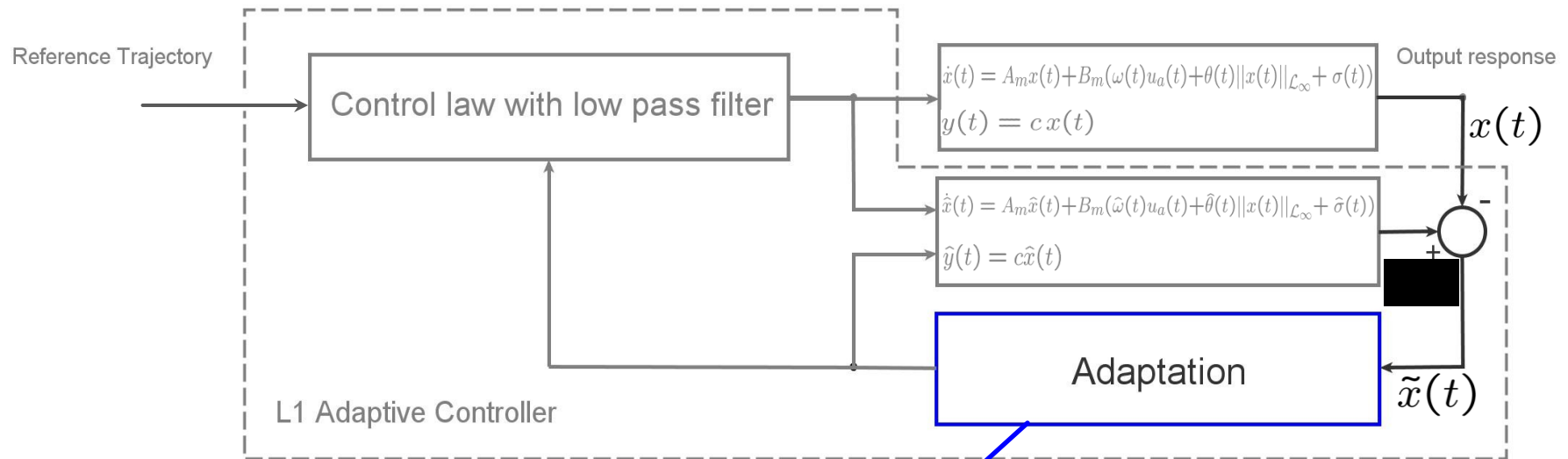
\mathcal{L}_1 Adaptive Controller Architecture



$$\dot{\hat{x}}(t) = A_m \hat{x}(t) + B_m(\hat{\omega}(t)u_a(t) + \hat{\theta}(t)\|\hat{x}(t)\|_{\mathcal{L}_\infty} + \hat{\sigma}(t))$$

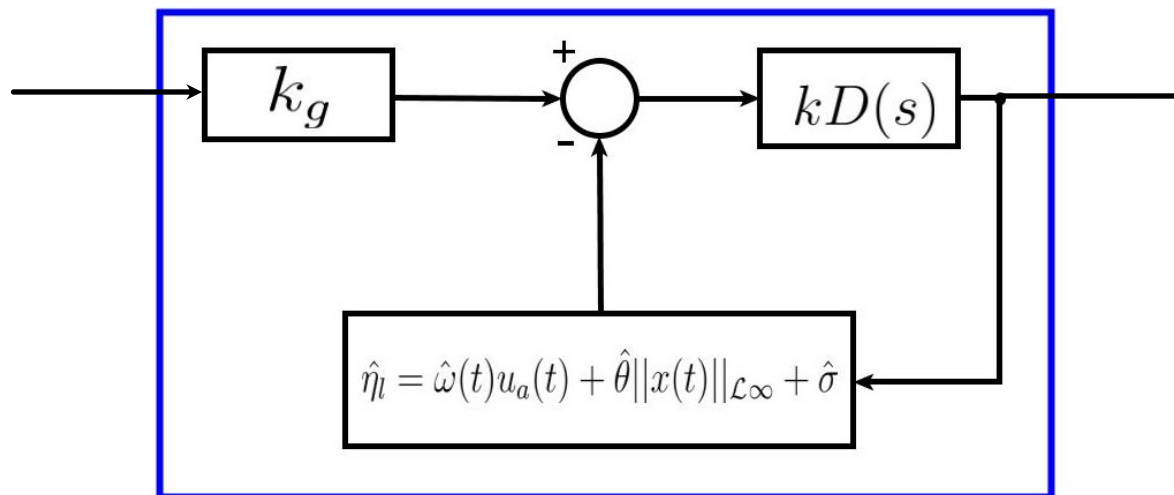
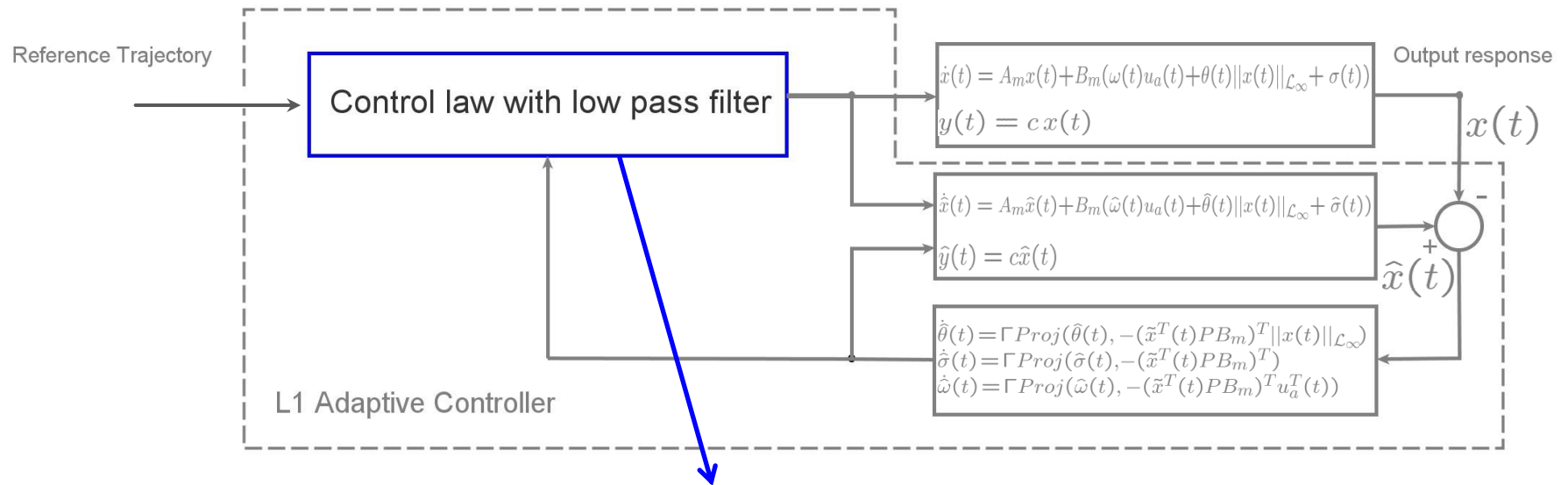
$$\hat{y}(t) = C\hat{x}(t)$$

\mathcal{L}_1 Adaptive Controller Architecture

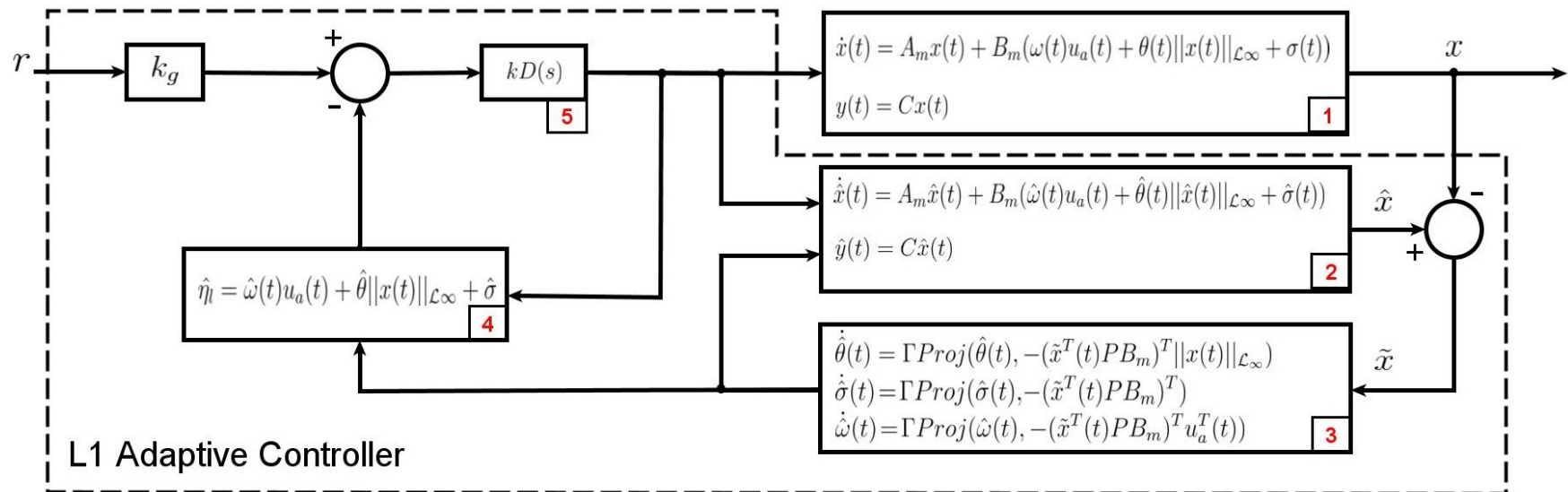


$$\begin{aligned}\dot{\hat{\theta}}(t) &= \Gamma Proj(\hat{\theta}(t), -(\tilde{x}^T(t) P B_m)^T \|x(t)\|_{\mathcal{L}_\infty}) \\ \dot{\hat{\sigma}}(t) &= \Gamma Proj(\hat{\sigma}(t), -(\tilde{x}^T(t) P B_m)^T) \\ \dot{\hat{\omega}}(t) &= \Gamma Proj(\hat{\omega}(t), -(\tilde{x}^T(t) P B_m)^T u_a^T(t))\end{aligned}$$

\mathcal{L}_1 Adaptive Controller Architecture



\mathcal{L}_1 Adaptive Controller Architecture Summary



- 1 Controlled system
- 2 Prediction phase
- 3 Parameter update
- 4- 5 Control input, with feedback gain k , pre-filter k_g and filter $D(s)$

Introduction

Controller

Modeling

Experiments

Conclusion

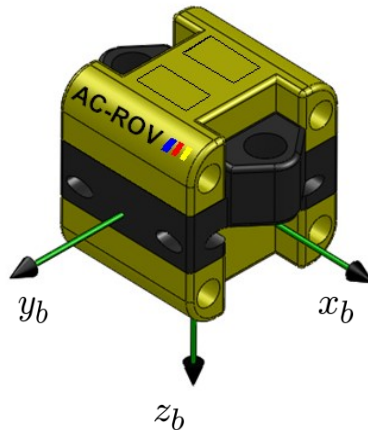
Modeling

Motion Variables for a Marine Vessel

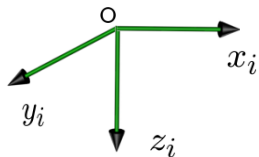
φ : rotation/ x_i

ψ : rotation/ y_i

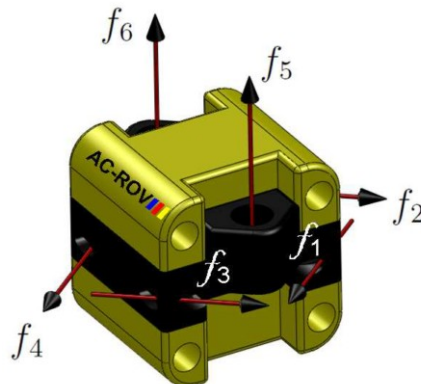
ϑ : Rotation/ z_i



Earth frame



Forces produced by the thrusters



Dynamic Modeling [Fossen2002]

$$M\dot{v} + C(v)v + D(v)v + G(\eta) = \tau + w_d$$

$$\dot{\eta} = J(\eta)v$$

$$v = [u \ v \ w \ p \ q \ r]^T$$

Vector of velocities in the body fixed frame

$$\eta = [x \ y \ z \ \varphi \ \vartheta \ \psi]^T$$

Vector of positions in the earth fixed frame

$$M, C(v), D(v)$$

Model matrices (Mass, Coriolis, Damping)

$$G(\eta)$$

Vector of gravitational / buoyancy forces

τ Vector of control inputs

w_d Vector of external disturbances

J Transformation matrix

Equation of dynamic model in the body-fixed frame

$$M\dot{v} + \cancel{C(\eta)v} + D(v)v + G(\eta) = \tau + w_d$$

$$\dot{\eta} = J(\eta)v$$

Equation of the reduced dynamic model in the earth-fixed frame

$$M_r^*(\eta)\ddot{\eta}_r + D_r^*(\eta)\dot{\eta}_r + g_r^*(\eta) = \tau_r^*(\eta) + w_{d_r}^*(\eta)$$

Studied Dynamics

Position of center of gravity

Weight

Buoyancy

$$\begin{bmatrix} M_z^* & 0 \\ 0 & M_\vartheta^* \end{bmatrix} \begin{bmatrix} \ddot{z} \\ \ddot{\vartheta} \end{bmatrix} + \begin{bmatrix} D_z^* & 0 \\ 0 & D_\vartheta^* \end{bmatrix} \begin{bmatrix} \dot{z} \\ \dot{\vartheta} \end{bmatrix} + \begin{bmatrix} -W \cos(\varphi) \sin(\vartheta) \\ W r_{g_z} \cos(\varphi) \sin(\vartheta) \end{bmatrix} = \begin{bmatrix} \tau_z^* + w_{d_z}^* \\ \tau_\vartheta^* + w_{d_\vartheta}^* \end{bmatrix}$$

Studied Dynamics

$$\begin{bmatrix} M_z^* & 0 \\ 0 & M_\vartheta^* \end{bmatrix} \begin{bmatrix} \ddot{z} \\ \ddot{\vartheta} \end{bmatrix} + \begin{bmatrix} D_z^* & 0 \\ 0 & D_\vartheta^* \end{bmatrix} \begin{bmatrix} \dot{z} \\ \dot{\vartheta} \end{bmatrix} + \begin{bmatrix} -(W - B) \\ W r_{gz} \cos(\varphi) \sin(\vartheta) \end{bmatrix} = \begin{bmatrix} \tau_z^* + w_{d_z}^* \\ \tau_\vartheta^* + w_{d_\vartheta}^* \end{bmatrix}$$

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State Space Representation of the Studied Dynamics

$$\begin{bmatrix} \dot{\eta}_1 \\ \dot{\eta}_2 \end{bmatrix} = \begin{bmatrix} 0_{2 \times 2} & \mathbb{I}_2 \\ 0_{2 \times 2} & \frac{-D_r^*}{M_r^*} \end{bmatrix} \begin{bmatrix} \eta_1 \\ \eta_2 \end{bmatrix} - \begin{bmatrix} 0_{2 \times 1} \\ \frac{g_r^*}{M_r^*} - \frac{w_{d_r}^*}{M_r^*} \end{bmatrix} + \begin{bmatrix} 0_{2 \times 2} \\ \frac{1}{M_r^*} \end{bmatrix} \omega \tau_r^*$$

$$\eta_1 = [z, \vartheta]^T \text{ and } \eta_2 = [\dot{z}, \dot{\vartheta}]^T$$

Studied Dynamics

$$\begin{bmatrix} M_z^* & 0 \\ 0 & M_\vartheta^* \end{bmatrix} \begin{bmatrix} \ddot{z} \\ \ddot{\vartheta} \end{bmatrix} + \begin{bmatrix} D_z^* & 0 \\ 0 & D_\vartheta^* \end{bmatrix} \begin{bmatrix} \dot{z} \\ \dot{\vartheta} \end{bmatrix} + \begin{bmatrix} -(W - B) \\ W r_{g_z} \cos(\varphi) \sin(\vartheta) \end{bmatrix} = \begin{bmatrix} \tau_z^* + w_{d_z}^* \\ \tau_\vartheta^* + w_{d_\vartheta}^* \end{bmatrix}$$

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\mathcal{L}_1 State Space Formulation

$$\begin{bmatrix} \dot{\eta}_1 \\ \dot{\eta}_2 \end{bmatrix} = A_m \begin{bmatrix} \eta_1 \\ \eta_2 \end{bmatrix} + \begin{bmatrix} 0_{2 \times 2} \\ \frac{1}{M_r^*} \end{bmatrix} (\omega u_a + \theta(t) \|\eta(t)\|_{\mathcal{L}_\infty} + \sigma(t))$$

$$y = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} \eta_1 \\ \eta_2 \end{bmatrix} = \begin{bmatrix} z \\ \vartheta \end{bmatrix}$$

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Introduction

Controller

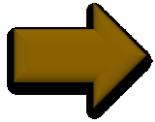
Modeling

Experiments

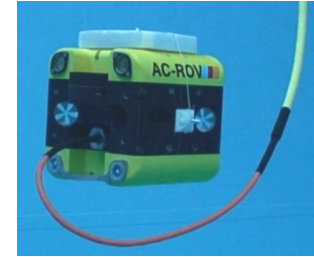
Conclusion

Experiments

Experimental Scenarios



Scenario 1
nominal conditions



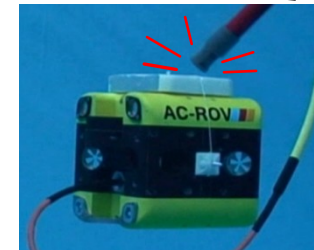
Scenario 2
robustness towards
uncertainties



added buoyancy



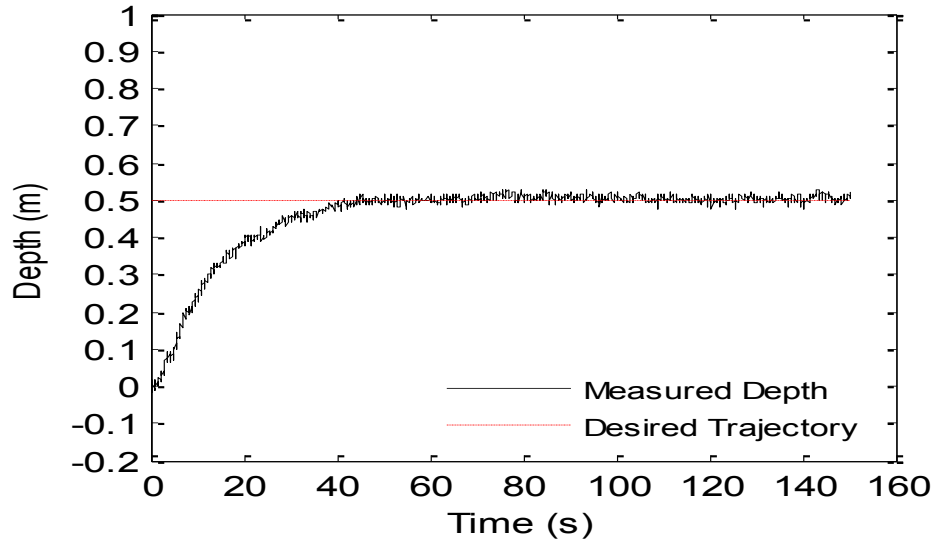
Scenario 3
external disturbances
rejection



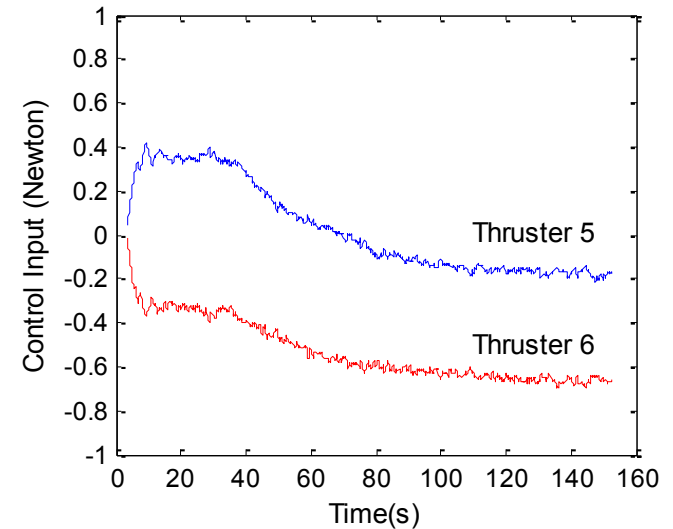
mechanical impact

Scenario 1 Nominal Conditions

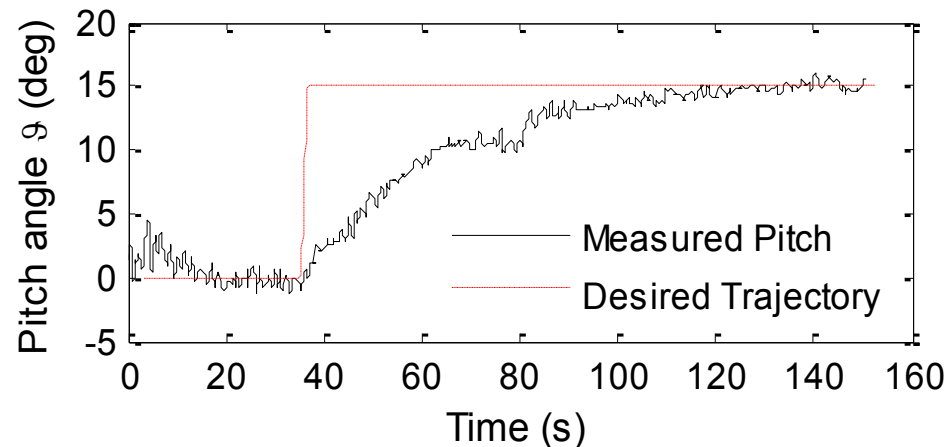
Depth (z)



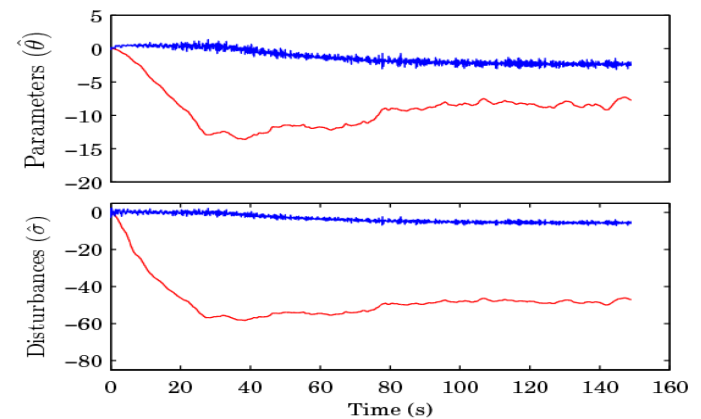
Control inputs



Pitch ϑ



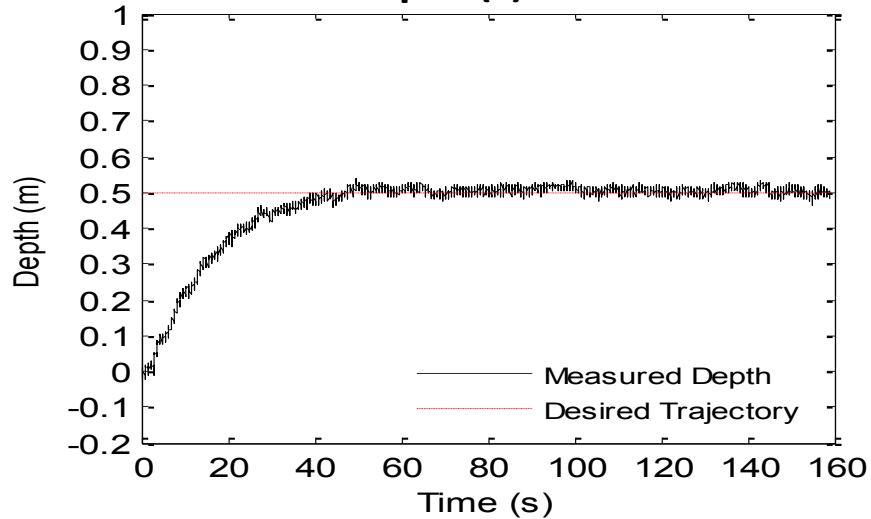
Estimated parameters and disturbances



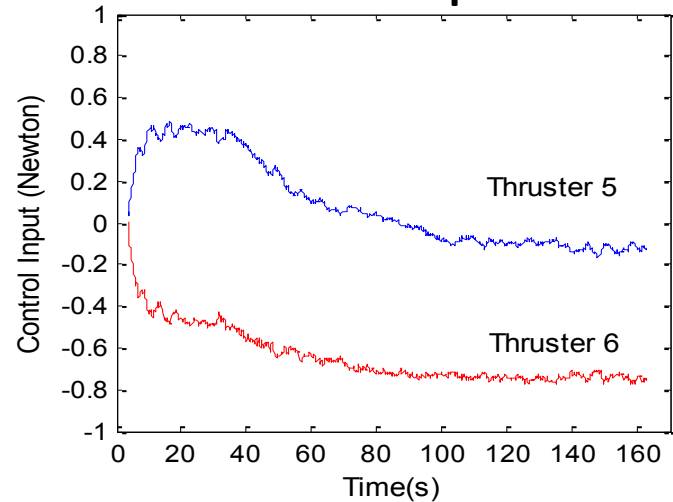
Scenario 2 Robustness Towards Parameter Uncertainties (Buoyancy Increase 32%)



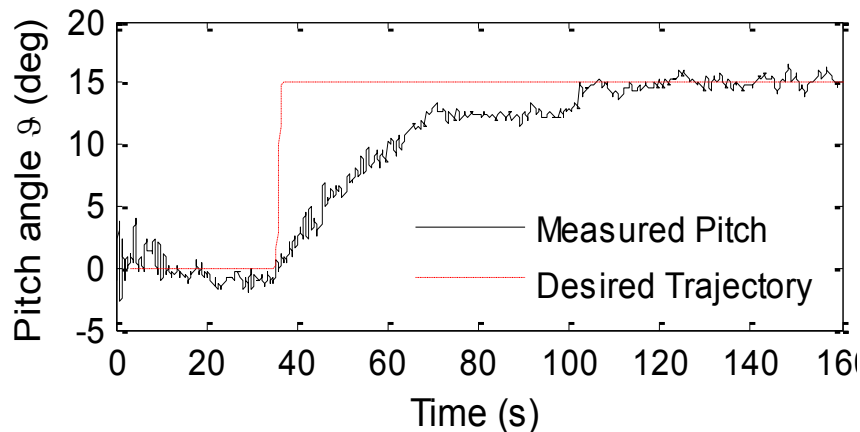
Depth (z)



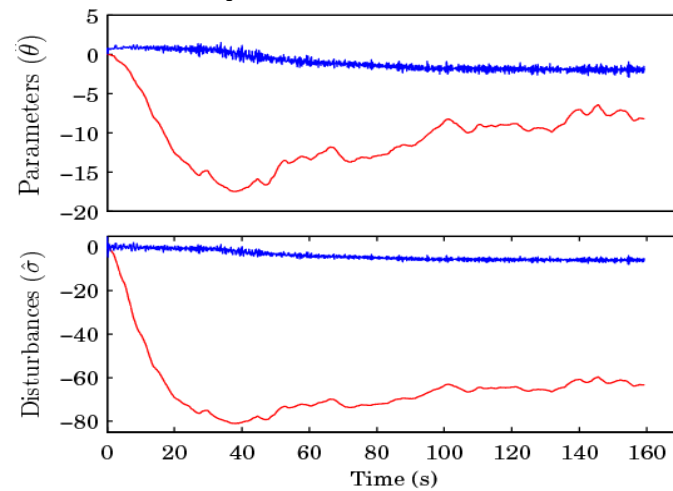
Control inputs



Pitch (ϑ)



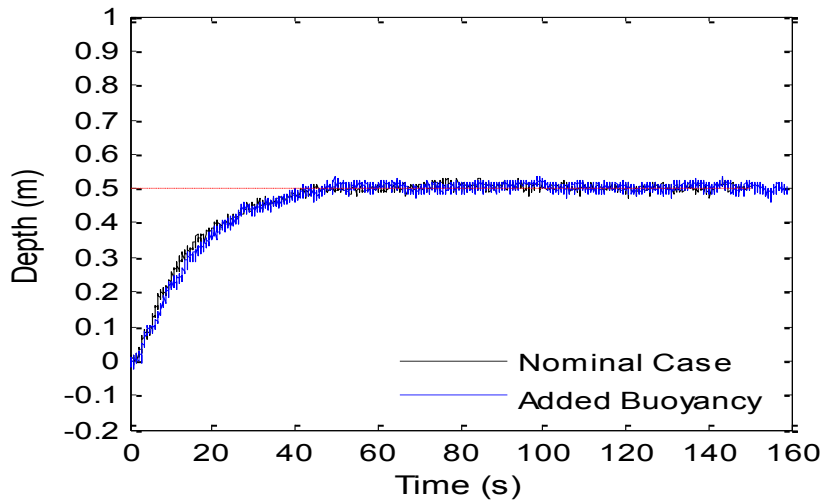
Estimated parameters and disturbances



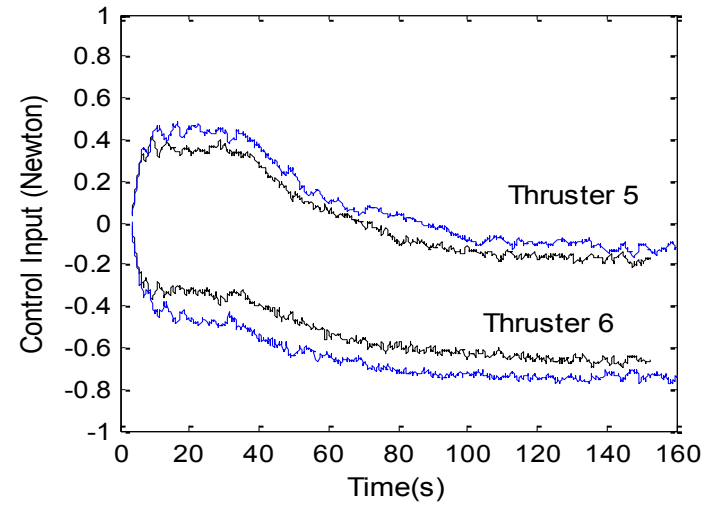
Scenarios 1 and 2 overlapped



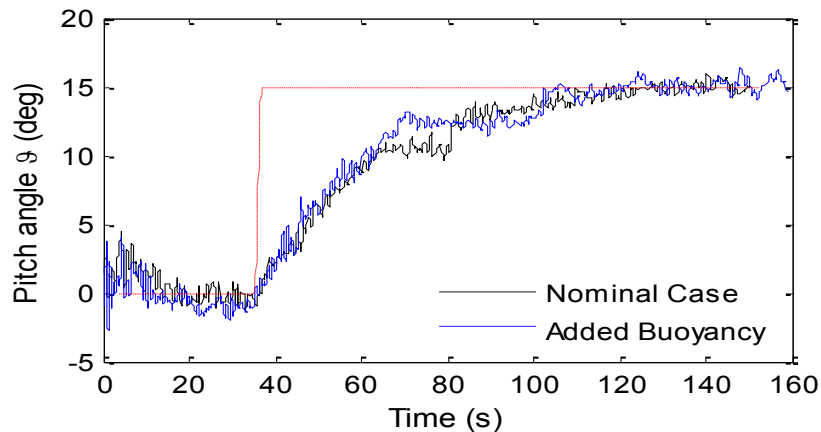
Depth (z)



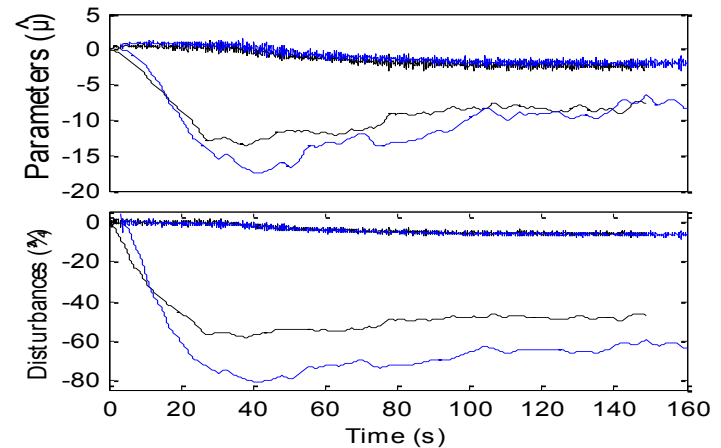
Control inputs



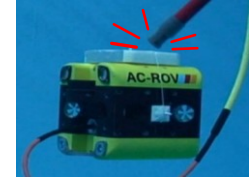
Pitch (ϑ)



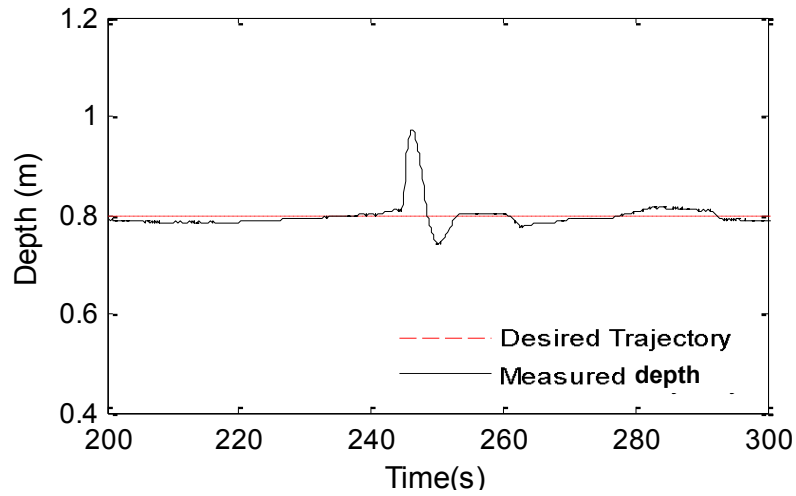
Estimated parameters and disturbances



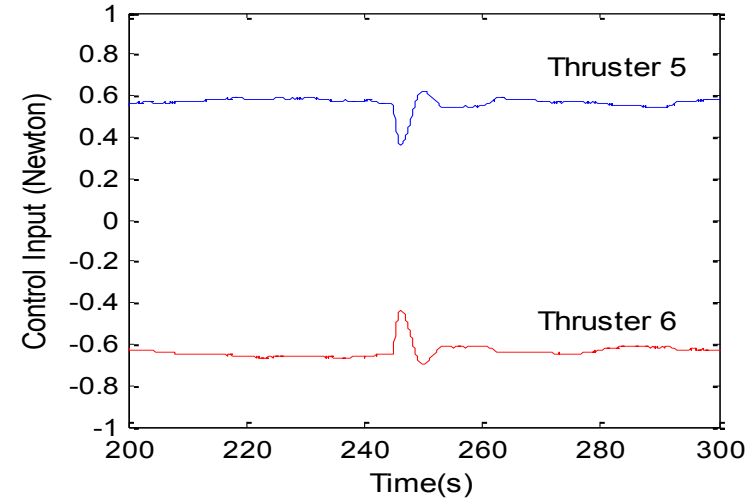
Scenario 3 External Disturbance Rejection (Punctual Disturbance)



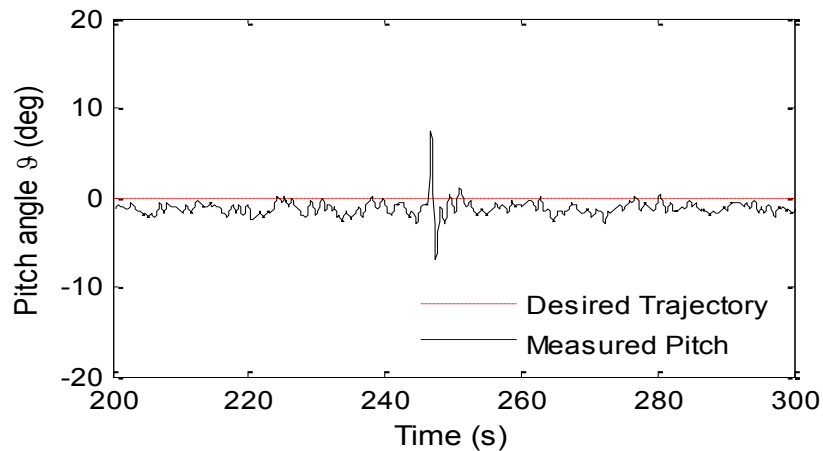
Depth (z)



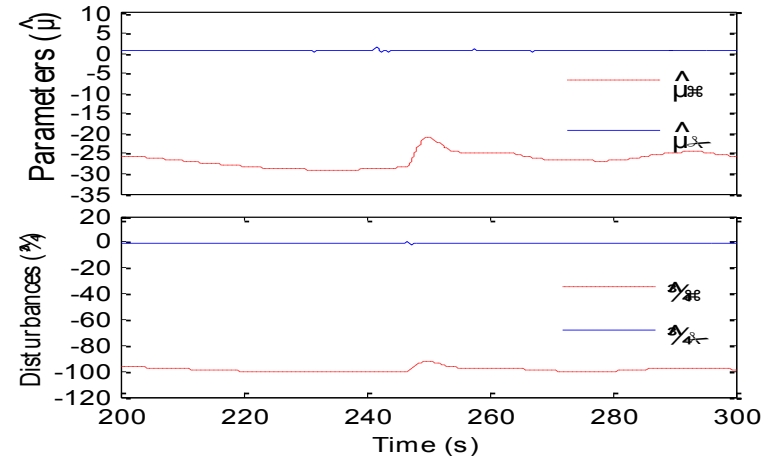
Control inputs




Pitch (ϑ)



Estimated parameters and disturbances





Laboratoire
d'Informatique
de Robotique
et de Microélectronique
de Montpellier

um2
UNIVERSITÉ MONTPELLIER 2
MONTPELLIER FRANCE

cnrs

tecnalia

**\mathcal{L} , adaptive depth control of an underwater vehicle
in presence of uncertainties and disturbances**

Divine Maalouf, Ahmed Chemori, Vincent Creuze, and Olivier Tempier
LIRMM, CNRS / Université Montpellier 2

<http://www.lirmm.fr/~creuze/UWR.htm>

Introduction

Controller

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Conclusion

Problem: Control of an underwater vehicle for trajectory tracking in presence of parameter uncertainties and external disturbances

Proposed Solution: \mathcal{L}_1 adaptive controller

Difficulties inherent to the system:

- High nonlinearities in the system's dynamics
- Variation of the model parameters
- Presence of external disturbances

Results: Experimental validation through various scenarios

Advantages of the proposed solution :

- Robustness and adaptation decoupled
- Usage of high adaptation gains
- Robustness towards uncertainties
- External disturbances rejection
- No a priori knowledge of the parameters is needed